

HYDROLOGY & HYDRAULICS STUDY

FOR

STARFISH

LOTS 1 TO 7 AND LOT A - TRACT 19115

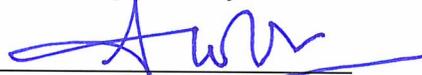
9779 STARFISH AVENUE

FOUNTAIN VALLEY, CALIFORNIA

Prepared For:

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February 22, 2021



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INTRODUCTION AND SUMMARY

Site Description

The proposed project is located at 9779 Starfish Avenue and encompasses 1.02 acres in the City of Fountain Valley. The project consists of construction of 7 single family homes. The site is bounded by existing residential properties to the north and west, vacant land to the east and Starfish Avenue to the south.

Existing Conditions

The proposed project is located along the northerly curb of Starfish Avenue, west of Mt. Henry Street. The overall site is relatively flat. The approximate elevations of the site vary from 28.0 to 32.0 feet above mean sea level (msl). Currently the site is fenced off landscape area with a basketball court. The site was initially owned by Huntington Valley Baptist church but has since been fenced off. Under existing conditions, the project drains to Starfish Avenue.

Proposed Conditions

To capture, store, and infiltrate storm water (low flow) runoff will be directed to Eco-Stone permeable pavers underlaid with open graded gravel in drive areas. The flow from permeable pavers will be directed to a bottomless trench drain. Overflow (high flow) from the area will be directed via a parkway drain to Starfish Avenue.

Purpose

The purpose of this study is to determine the runoff generated by a storm of 10-year, 25-year and 100-year frequency for both existing and proposed conditions. The site drainage will be designed for a 25-year storm. The attached parkway culvert calculations show that the culverts have the capacity for a storm event of 10-year frequency.

Methodology

The hydrology calculations have been prepared using the A.E.S. Program based on the 1986 Orange County Hydrology Manual.

Soil Type

The soil type is Type "D" as determined from Plate A of the Hydrology Manual.

Land Use

For existing conditions the watershed was taken as a church/school. For proposed conditions the watershed was taken as a single-family residential development.

Conclusion

The table below summarizes the total runoff from the site for a storm of 10-year, 25-year and 100-year frequency.

	Existing Conditions	Proposed Conditions
10-Year Storm Event	2.04 cfs	2.22 cfs
25-Year Storm Event	2.47 cfs	2.68 cfs
100-Year Storm Event	3.19 cfs	3.44 cfs

The run-off indicated in the table above is the raw number and does not account from infiltration to permeable pavers.

Under proposed condition, the run-off from the site is directed to permeable pavers over open graded gravel for infiltration as required by Orange County drainage area Management plan (DAMP). Only the overflow from the site after infiltration outlets via parkway drain to existing curb & gutter on Starfish Avenue.

RATIONAL METHOD HYDROLOGY

Existing Conditions

10-Year Storm Event

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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Analysis prepared by:
DMS Consultants, inc.

FILE NAME: STAR10.DAT
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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 10.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- CROWN TO		STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES:			MANNING FACTOR (n)
	WIDTH (FT)	CROSSFALL (FT)			WIDTH (FT)	LIP (FT)	HIKE (FT)	
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 375.00
ELEVATION DATA: UPSTREAM(FEET) = 31.90 DOWNSTREAM(FEET) = 28.25

$T_c = K * [(LENGTH^{**} 3.00) / (ELEVATION CHANGE)]^{**} 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 12.680
* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.382
SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
RESIDENTIAL "1 DWELLING/ACRE"	D	1.02	0.20	0.800	57	12.68

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.800
SUBAREA RUNOFF(CFS) = 2.04
TOTAL AREA(ACRES) = 1.02 PEAK FLOW RATE(CFS) = 2.04
=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES)	=	1.02	TC (MIN.)	=	12.68
EFFECTIVE AREA (ACRES)	=	1.02	AREA-AVERAGED F_m (INCH/HR)	=	0.16
AREA-AVERAGED F_p (INCH/HR)	=	0.20	AREA-AVERAGED A_p	=	0.800
PEAK FLOW RATE (CFS)	=	2.04			

=====
=====
END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY

Existing Conditions

25-Year Storm Event

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
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---*TIME-OF-CONCENTRATION MODEL*---

USER SPECIFIED STORM EVENT(YEAR) = 25.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP (FT) (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 375.00
ELEVATION DATA: UPSTREAM(FEET) = 31.90 DOWNSTREAM(FEET) = 28.25

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 12.680
* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 2.849
SUBAREA T_c AND LOSS RATE DATA(AMC I):
DEVELOPMENT TYPE/ LAND USE SCS SOIL AREA Fp Ap SCS Tc
GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"1 DWELLING/ACRE" D 1.02 0.20 0.800 57 12.68
SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.800
SUBAREA RUNOFF(CFS) = 2.47
TOTAL AREA(ACRES) = 1.02 PEAK FLOW RATE(CFS) = 2.47
=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES)	=	1.02	TC (MIN.)	=	12.68
EFFECTIVE AREA (ACRES)	=	1.02	AREA-AVERAGED F_m (INCH/HR)	=	0.16
AREA-AVERAGED F_p (INCH/HR)	=	0.20	AREA-AVERAGED A_p	=	0.800
PEAK FLOW RATE (CFS)	=	2.47			

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END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY

Existing Conditions

100-Year Storm Event

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--*TIME-OF-CONCENTRATION MODEL*--
=====

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP (FT) (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 375.00
ELEVATION DATA: UPSTREAM(FEET) = 31.90 DOWNSTREAM(FEET) = 28.25

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 12.680
* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.630
SUBAREA T_c AND LOSS RATE DATA (AMC I):
DEVELOPMENT TYPE/ LAND USE SCS SOIL GROUP AREA (ACRES) F_p (INCH/HR) A_p (DECIMAL) SCS CN T_c (MIN.)
RESIDENTIAL
"1 DWELLING/ACRE" D 1.02 0.20 0.800 57 12.68
SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.800
SUBAREA RUNOFF (CFS) = 3.19
TOTAL AREA (ACRES) = 1.02 PEAK FLOW RATE (CFS) = 3.19
=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES)	=	1.02	TC (MIN.)	=	12.68
EFFECTIVE AREA (ACRES)	=	1.02	AREA-AVERAGED F_m (INCH/HR)	=	0.16
AREA-AVERAGED F_p (INCH/HR)	=	0.20	AREA-AVERAGED A_p	=	0.800
PEAK FLOW RATE (CFS)	=	3.19			

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END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY

Proposed Conditions

10-Year Storm Event

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
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---*TIME-OF-CONCENTRATION MODEL*---

USER SPECIFIED STORM EVENT(YEAR) = 10.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP (FT) (FT)	MANNING HIKE (FT) (n)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 365.00
ELEVATION DATA: UPSTREAM(FEET) = 33.10 DOWNSTREAM(FEET) = 29.75

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 11.150

* 10 YEAR RAINFALL INTENSITY(INCH/HR) = 2.564

SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
RESIDENTIAL "3-4 DWELLINGS/ACRE"	D	1.01	0.20	0.600	57	11.15

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.600

SUBAREA RUNOFF(CFS) = 2.22

TOTAL AREA(ACRES) = 1.01 PEAK FLOW RATE(CFS) = 2.22
=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES)	=	1.01	TC (MIN.)	=	11.15
EFFECTIVE AREA (ACRES)	=	1.01	AREA-AVERAGED F _m (INCH/HR)	=	0.12
AREA-AVERAGED F _p (INCH/HR)	=	0.20	AREA-AVERAGED A _p	=	0.600
PEAK FLOW RATE (CFS)	=	2.22			

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END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY

Proposed Conditions

25-Year Storm Event

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 25.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 365.00
ELEVATION DATA: UPSTREAM(FEET) = 33.10 DOWNSTREAM(FEET) = 29.75

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 11.150

* 25 YEAR RAINFALL INTENSITY(INCH/HR) = 3.064

SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
RESIDENTIAL "3-4 DWELLINGS/ACRE"	D	1.01	0.20	0.600	57	11.15

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20

SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.600

SUBAREA RUNOFF(CFS) = 2.68

TOTAL AREA(ACRES) = 1.01 PEAK FLOW RATE(CFS) = 2.68
=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES)	=	1.01	TC (MIN.)	=	11.15
EFFECTIVE AREA (ACRES)	=	1.01	AREA-AVERAGED F_m (INCH/HR)	=	0.12
AREA-AVERAGED F_p (INCH/HR)	=	0.20	AREA-AVERAGED A_p	=	0.600
PEAK FLOW RATE (CFS)	=	2.68			

=====
=====
END OF RATIONAL METHOD ANALYSIS

RATIONAL METHOD HYDROLOGY

Proposed Conditions

100-Year Storm Event

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 4.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) I ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
 2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
- *SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 101.00 TO NODE 102.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 365.00
ELEVATION DATA: UPSTREAM(FEET) = 33.10 DOWNSTREAM(FEET) = 29.75

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 11.150
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.908
SUBAREA T_c AND LOSS RATE DATA(AMC I):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
RESIDENTIAL "3-4 DWELLINGS/ACRE"	D	1.01	0.20	0.600	57	11.15

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.20
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.600
SUBAREA RUNOFF(CFS) = 3.44
TOTAL AREA(ACRES) = 1.01 PEAK FLOW RATE(CFS) = 3.44
=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES)	=	1.01	TC (MIN.)	=	11.15
EFFECTIVE AREA (ACRES)	=	1.01	AREA-AVERAGED F_m (INCH/HR)	=	0.12
AREA-AVERAGED F_p (INCH/HR)	=	0.20	AREA-AVERAGED A_p	=	0.600
PEAK FLOW RATE (CFS)	=	3.44			

=====
=====
END OF RATIONAL METHOD ANALYSIS

HYDRAULICS
Parkway Culverts Capacity Calculations

HYDRAULIC ELEMENTS - I PROGRAM PACKAGE
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Analysis prepared by:

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TIME/DATE OF STUDY: 15:42 03/02/2021
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Problem Descriptions:
Parkway Drain Calcs

>>>>CHANNEL INPUT INFORMATION<<<<

NORMAL DEPTH (FEET) = 0.33
CHANNEL Z1 (HORIZONTAL/VERTICAL) = 0.00
Z2 (HORIZONTAL/VERTICAL) = 0.00
CONSTANT CHANNEL SLOPE (FEET/FEET) = 0.009000
UNIFORM FLOW (CFS) = 2.68
MANNINGS FRICTION FACTOR = 0.0130
=====

NORMAL-DEPTH FLOW INFORMATION:

>>>>> BASEWIDTH (FEET) = 1.91 -----> OK (Provided 2.0')
FLOW TOP-WIDTH (FEET) = 1.91
FLOW AREA (SQUARE FEET) = 0.63
HYDRAULIC DEPTH (FEET) = 0.33
FLOW AVERAGE VELOCITY (FEET/SEC.) = 4.25
UNIFORM FROUDE NUMBER = 1.304
PRESSURE + MOMENTUM (POUNDS) = 28.56
AVERAGED VELOCITY HEAD (FEET) = 0.280
SPECIFIC ENERGY (FEET) = 0.610
=====

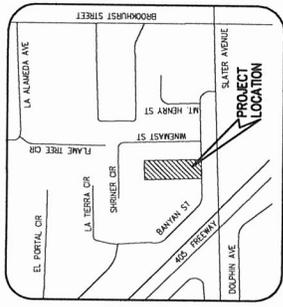
CRITICAL-DEPTH FLOW INFORMATION:

CRITICAL FLOW TOP-WIDTH (FEET) = 1.91
CRITICAL FLOW AREA (SQUARE FEET) = 0.75
CRITICAL FLOW HYDRAULIC DEPTH (FEET) = 0.39
CRITICAL FLOW AVERAGE VELOCITY (FEET/SEC.) = 3.55
CRITICAL DEPTH (FEET) = 0.39
CRITICAL FLOW PRESSURE + MOMENTUM (POUNDS) = 27.74
AVERAGED CRITICAL FLOW VELOCITY HEAD (FEET) = 0.196
CRITICAL FLOW SPECIFIC ENERGY (FEET) = 0.591
=====

APPENDIX

Hydrology Maps

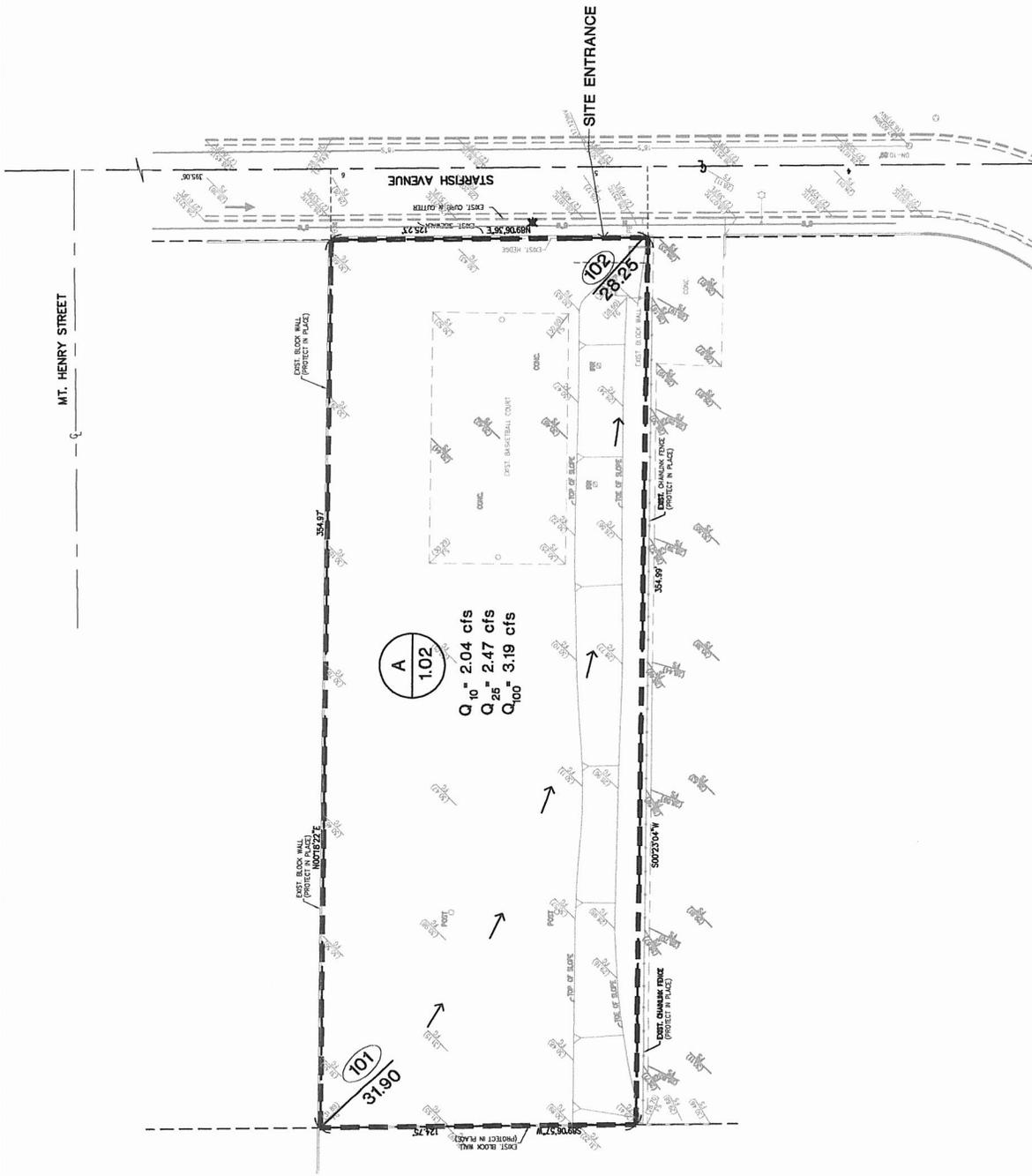
Existing and Proposed Conditions



VICINITY MAP
NOT TO SCALE

LEGEND

	AREA DESIGNATION
	AREA IN ACRES
	NODE DESIGNATION
	ELEVATION
	DIRECTION OF FLOW



A
1.02
Q₁₀ = 2.04 cfs
Q₂₅ = 2.47 cfs
Q₁₀₀ = 3.19 cfs

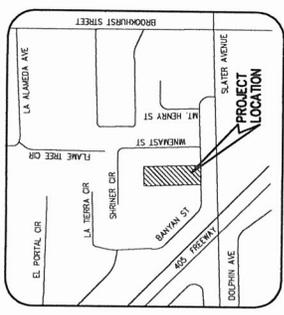
OWNER/DEVELOPER:
STARFISH FV VENTURE, LLC

ENGINEER:
DMS CONSULTANTS, INC.
C. J. DAVIS, P.E.
10711 Lakeside Blvd., Suite 200, San Diego, CA 92123
TEL: 619-594-8800 FAX: 619-594-8801

PREPARED UNDER THE SUPERVISION OF:
Andrew M. DeWan
SURVEYOR M. DEWAN

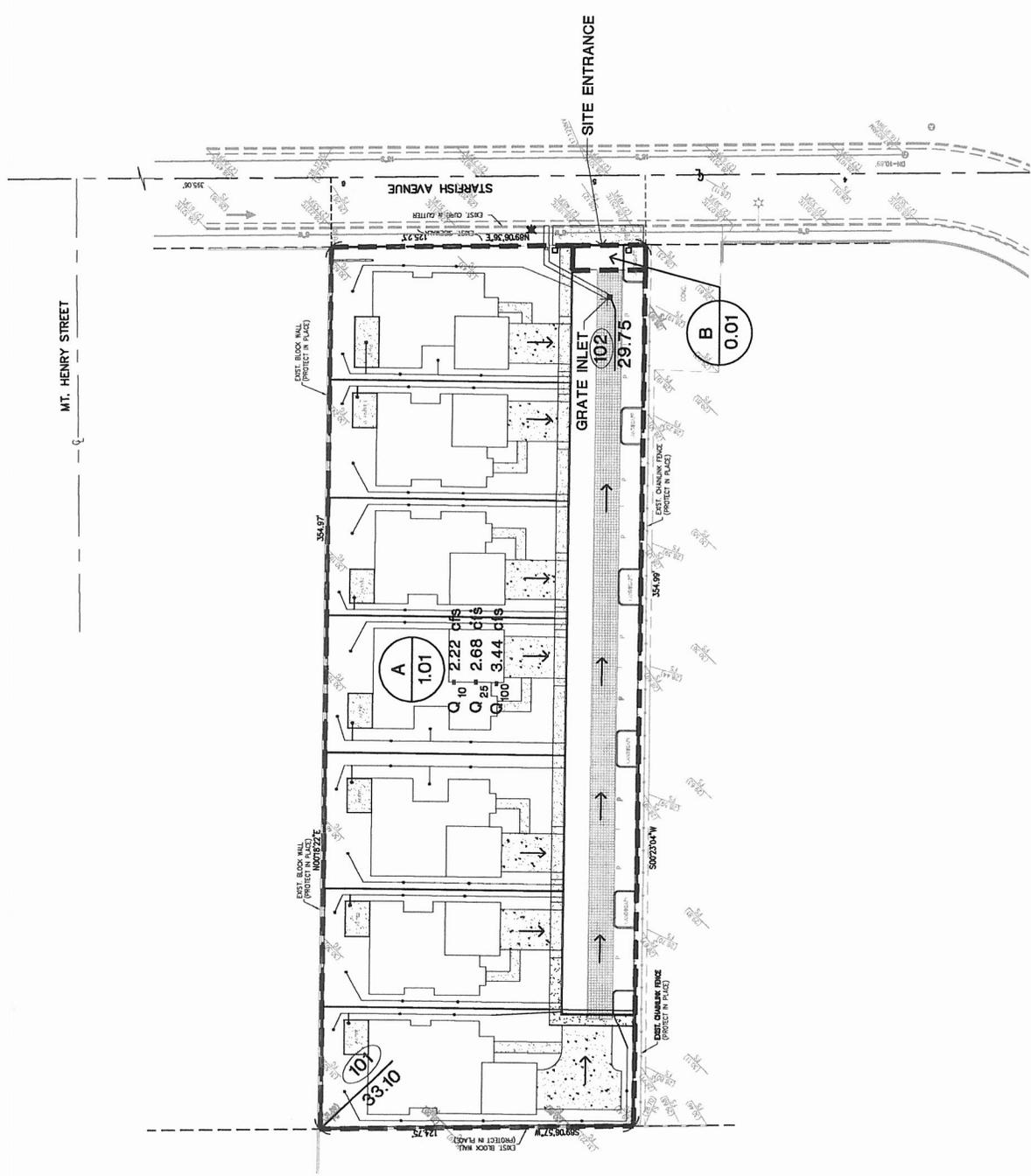
CITY OF FOUNTAIN VALLEY
HYDROLOGY PLAN - EXISTING CONDITIONS
TENTATIVE TRACT NO. 19115
9779 STARFISH AVENUE, FOUNTAIN VALLEY, CA 92708
DATE: 02/19/2021

SCALE: 1"=20'



LEGEND

A	AREA DESIGNATION
0.00	AREA IN ACRES
XXX	NODE DESIGNATION
45.00	ELEVATION
←	DIRECTION OF FLOW



OWNER/DEVELOPER:
STARFISH FV VENTURE, LLC

DMS
CONSULTANTS INC
CIVIL ENGINEERS
1271 Linn St. Red Bluff, GA 30465 P: 770-762-8182



PREPARED UNDER THE SUPERVISION OF
ANDAK
SURINDER N. DEWAN

SCALE: 1"=20'

CITY OF FOUNTAIN VALLEY
HYDROLOGY PLAN - PROPOSED CONDITIONS
TENTATIVE TRACT NO. 19115
9779 STARFISH AVENUE, FOUNTAIN VALLEY, CA 92708
DATE: 02/19/2021

SHEET 1 OF 1